### DTU

### Ram Pump Programme

DTU P90 PUMP

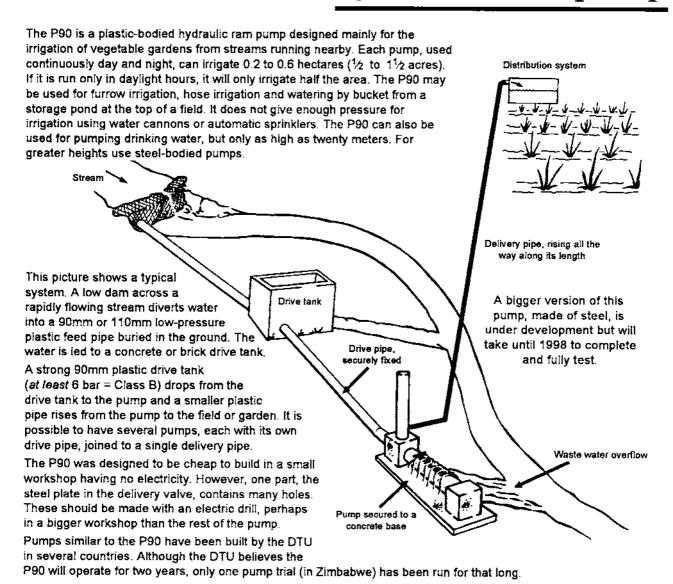
TECHNICAL

12
RELEASE

### DTU P90

The name "P90" stands for a Plastic pump with a drive pipe of 90mm in diameter.

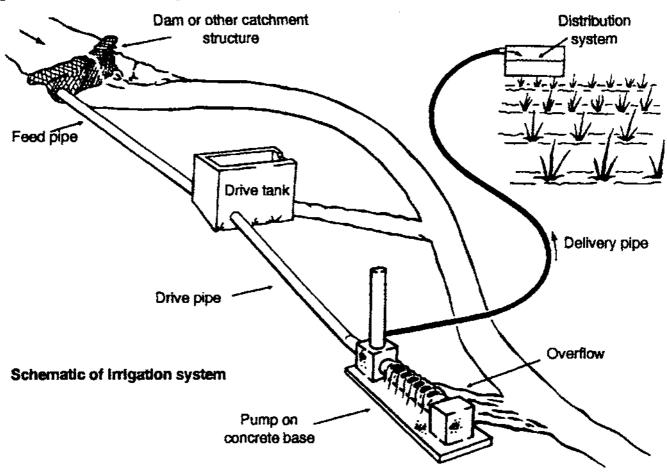
### hydraulic ram pump



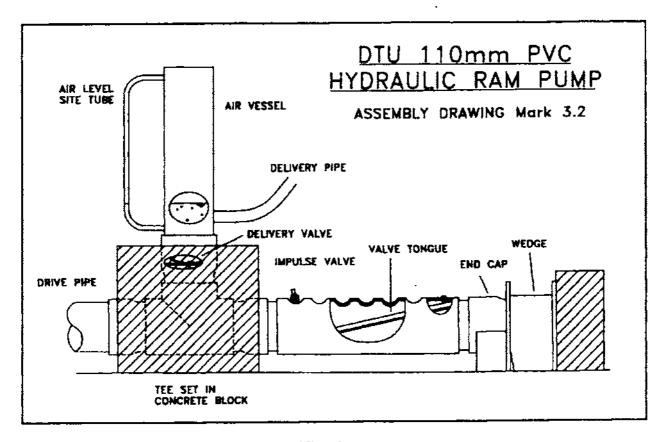
### DTU P90 ram pump specifications The normal specifications of the DTU P90 ram pump are given here. Sometimes you can operate pumps outside these limits, but they may not work well. drive head range up to 3 meters drive flow range 100 to 360 liters a minute drive pipe material PVC or ABS (at least 6 per of Class B) drive pipe diameter 90mm delivery head range up to 20 meters typical delivery range 3 to 40 liters a minute delivery pipe diameter 25mm

### The DTU plastic irrigation pump

Most ram pumps being manufactured are designed to supply water for domestic use because the low flows produced and the costs generally make ram pump systems unsuitable for small-scale crop irrigation. Sufficient water for 1000-1500 people, for example, would only irrigate a plot of around 1 hectare! Some very large bore (12") ram pumps have been built to supply water for irrigation but the capital costs of such schemes restricts their application. In many parts of the world there is a large potential for low-lift, low-cost irrigation of small garden plots to improve yields, allow alternative crops to be grown and increase crop security in unpredictable weather conditions.



The material the DTU selected as the only viable alternative to steel is plastic pipe. PVC 110mm (4") diameter pipe is now widely available in many developing countries and provides the scale of flow necessary for small-scale irrigation.



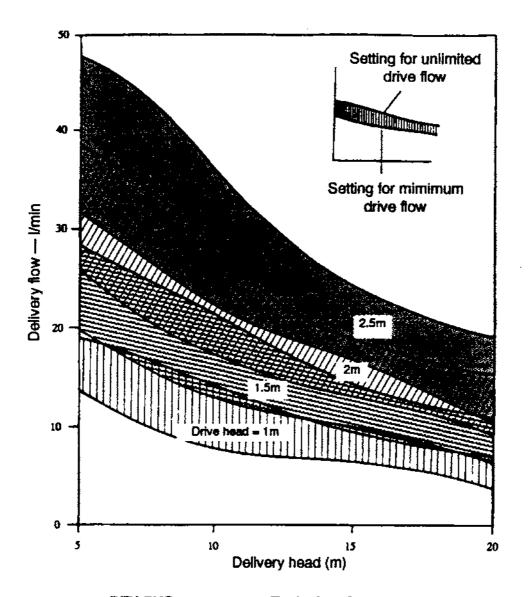
### The DTU pump has the following specification:

- all major parts can be manufactured from 110mm pipe (with a minimum of other materials such as bolts, rubber, etc.);
- all parts can be manufactured using hand tools in small rural workshops;
- n the system can be maintained by the user and all parts are capable of simple replacement in case of wear, damage or theft;
- designs have been extensively tested for performance and endurance (including extensive field tests);
- u pumps should be easy to tune to suit a broad range of site conditions.

### It meets the following performance specifications:

- The drive head (fall of water) can be between 1 and 3 metres.
- [2] The drive flow available can be between 3 and 7 litres/second.
- 3 The maximum delivery head is 12m.
- 4 The energy efficiency exceeds 50%.

At 2 metres drive head, maximum delivery to 15 metres is 35,000 litres per day, adequate to irrigate 2/3 of a hectare.



DTU PVC ram pump — Typical performance data

The shaded areas on the performance data chart above indicate the normal operating range for different values of drive head.

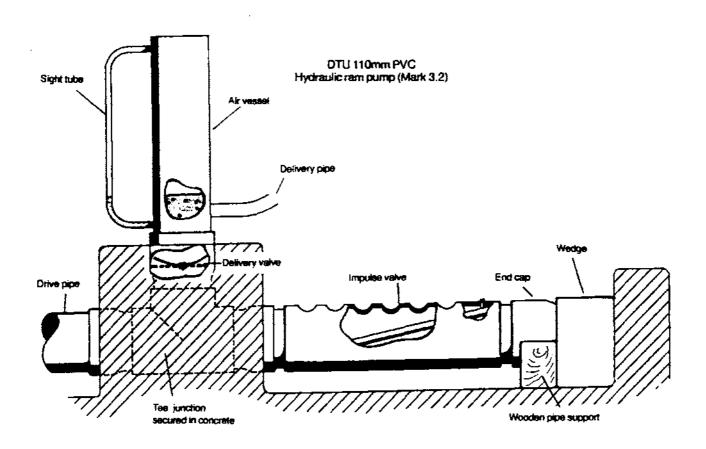
Pump designs have been developed over a number of years with increasing performance and component life. Plastic pipe is more prone to fatigue failure than steel, reducing the life of some components to two years. The current design has been extensively tested in Zimbabwe but is still (1993) at the proving stage of development.

### Manufacturing notes

The first DTU ram pump to be built using plastic materials was tested in 1986 as part of an undergraduate project. It was constructed largely from standard PVC drain pipe fittings with a wooden impulse valve. The major interest in the use of plastic for ram pumps stemmed from the low cost of materials and the ease of manufacture using plastic components. There was some question initially whether the thin PVC material would withstand the continual fatigue loading and simply break under the first cycles. With the success of this first design, research was continued on its development and the horizontal axis impulse valve was introduced. Since then laboratory tests and field trials have significantly refined the design of the pump and produced data concerning its durability and pumping limitations.

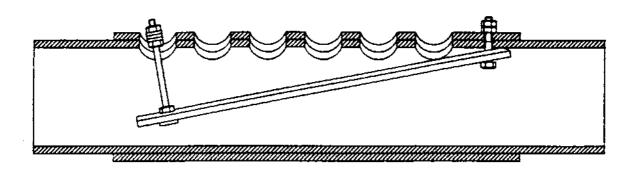
Plastic ram pumps can provide a cheap and simple means of supplying water to elevations of less than 15m. The scale of flow produced and the limitations on their pumping head make them ideal for local manufacture and use for small scale irrigation in developing countries.

This Working Paper details the design of the M3.2 pump. It lists each component and describes any significant features and considerations. Drawings of all the components are also included along with some graphs showing the typical performance of the pump.



### Impulse Valve

The design of impulse valve on the DTU M3.2 is unique amongst current ram pump designs. It aims to achieve a flow area through the valve equal to, or greater than, the area of the drive pipe whilst using the drive pipe material for its construction. This greatly simplifies the materials required for pump construction and reduces the need for steel components.



The M3.2 impulse valve

The valve operates under conditions similar to those that cause the aerodynamic lift of an aircraft wing. The velocity of the water flowing over the top of the tongue and out to waste, creates a slightly lower pressure on the top side than that underneath it. As the water accelerates, this pressure differential across the tongue increases until it is sufficient to begin to close the valve. As the tongue rises the velocity over it is increased, which in turn increases the pressure differential, causing the valve to close faster and further increasing the velocity. In this way the tongue accelerates and closes very rapidly producing the sudden deceleration of the water necessary to raise the pressure in the pump body to the delivery pressure.

The valve design works well using PVC materials due to its slight flexibility. When the valve closes the subsequent pressure rise actually flexes the tongue ensuring a good seal even though the tongue may not fit perfectly to the valve body. The same valve design has been tried using steel pipe material but was found not to work well as the tongue could not easily be contoured to the exact shape of the inside of the valve body and didn't have sufficient flexibility to deform under the normal working pressure. Provided that the tongue of a PVC pump fits sufficiently well to just operate it will deform over a number of days of operation until it seals properly.

The development of the this design from the basic concept has taken some time in using different configurations; hole sizes, spacing, valve length and in finding a design with sufficient strength to withstand the continual loading. PVC is not a material recommended for use in situations where a high fatigue loading is likely. Its use would therefore not normally be advisable in ram pumps where there is a highly fluctuating load from the pressure transients in the pump and drive pipe. Research has shown that provided the delivery pressure is kept within recommended limits, the pump and pipe material are sufficiently thick, and the pump well manufactured with no potential stress concentrators, that the normal fatigue loading experienced is well within the tolerance of the material. A Working Paper is available from the DTU detailing the research and findings of work undertaken on fatigue in PVC.

### Impulse Valve Design and Manufacture Notes

- 1) Great care is needed in the manufacture of the holes in the valve body to ensure that there are no small cuts, indentations or cracks from the initial shaping of the holes. Once the holes have been roughly shaped they should be carefully filed until they are completely smooth to the touch and show no visual defects. This will help prevent the formation and propagation of cracks.
- 2) The tongue hinge is a potential source of rapid wear of the PVC material used both for the tongue and the valve body. The hinge is simply a bolt about which the tongue has some freedom to move. To prevent wear of the tongue, the hole that goes through it is lined with a piece of metal, either a small section of pipe with the correct I/D or a specially fabricated liner made from sheet seed.
- 3) On two occasions impulse valve cracks were found running down the valve parallel to the pipe axis at the upstream end that was pushed into the tee piece. These cracks were caused by the valve being wedged too hard into the tee piece socket. This created a significant additional hoop stress at that end of the valve and led to a crack propagating from some small imperfection in the first valve hole back to the end of the pipe. The main cause of this problem was the method of wedging the impulse valve into the tee piece against the concrete end block. It is possible to prevent this type of cracking by wedging the impulse valve more carefully. However this does not provide a fool proof solution and still allows the possibility of valve failure. The simplest method of preventing this problem is to shorten the length of the pipe that can fit into the tee socket so that the double skin of the impulse valve butts up against the tee before the valve is pushed in too tight.

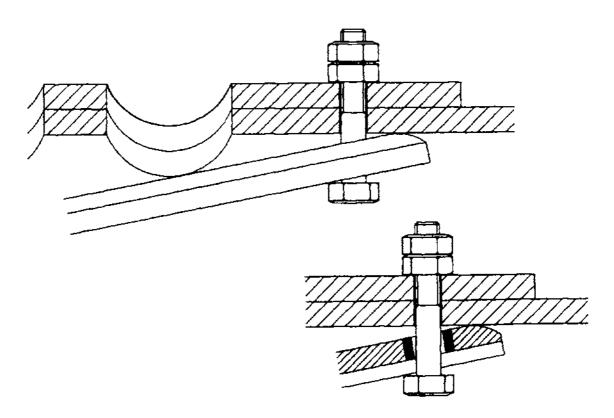
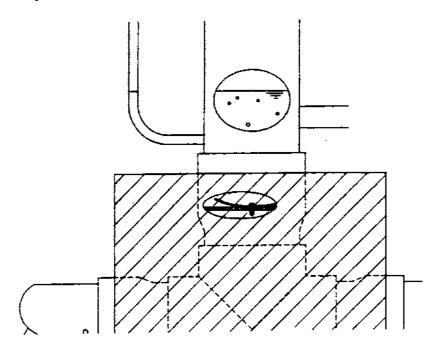


Diagram showing hinge arrangement of impulse valve tongue

### **Delivery Valve Design**

The delivery valve for a low cost ram pump must satisfy all of the following requirements;

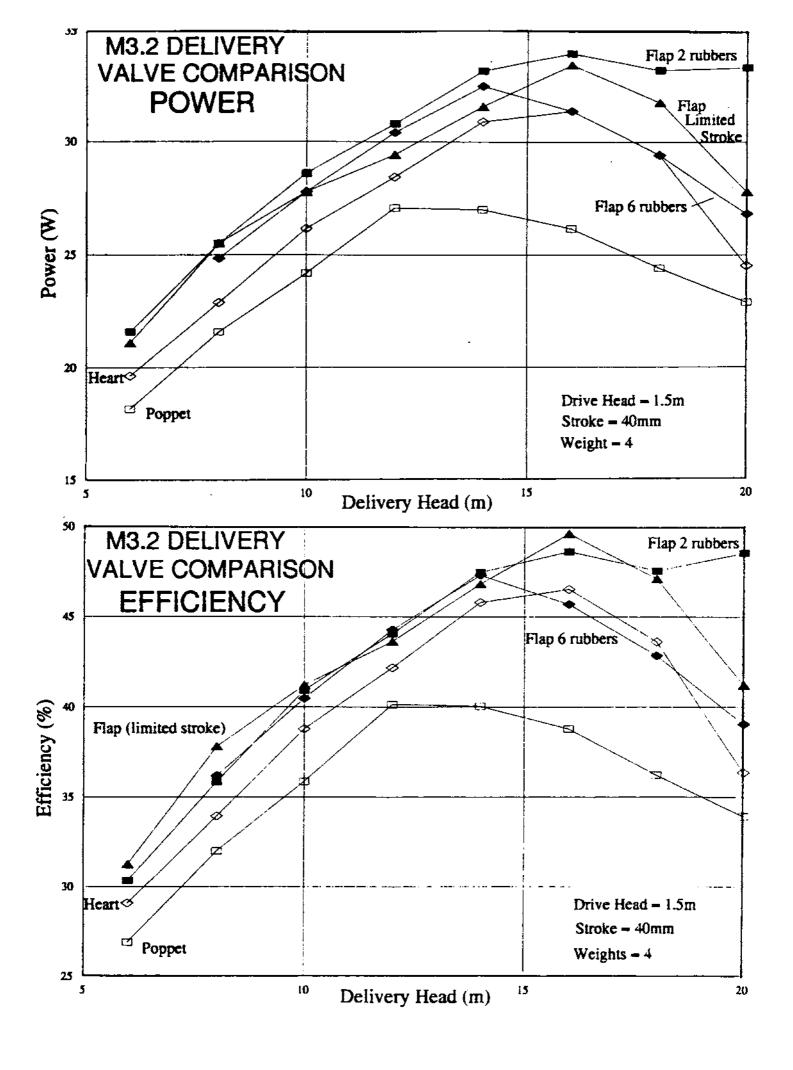
- 1) produce good performance by; opening quickly with a low pressure differential across it; have a low resistance to flow through it; allow little backflow by closing quickly with a small pressure differential.
- 2) have an acceptable working life with any disposable rubber parts lasting a minimum of 6 months.
- 3) be cheap and simple to manufacture.



Position of the Delivery Valve

Laboratory tests have been carried out on a number of different types of delivery valve to assess their performance. These were simply designed to compare the throughput of the valve under a controlled set of conditions. Backflow of water through the valve from the air vessel during the period of recoil had been found to be significant on tests of steel ram pumps, reducing the delivery flow by up to 40% in the worst cases. With identical impulse valve settings, the delivery head and flows were measured for 5 different delivery valves. The results of the tests are shown in the following graphs.

The original flap type delivery valve proved to give the best performance over a wide range of conditions with two thicknesses of rubber to increase the rigidity of the valve. The rubber used in the tests was 3mm thick commercial sheet. One thickness of rubber gives lower performance due to its lower response to closure allowing more backflow to occur. Increasing the number of rubbers above 2 also reduces the delivery flow as the resistance of the valve to opening increases and the friction through the valve during delivery reduces the flow. Unfortuneately the quality and availability of rubber sheet varies enormously around the world and it is important to be able to make use of locally available materials to guarantee access to spare parts. Good quality inner tube from truck wheels is often the most available and reliable source of rubber. It is recommended that a number of thicknesses be used to make the total thickness of rubber between 4 and 6mm. Some experimentation with the materials available is advised, measuring performance with varying amounts of rubber to find an optimum and assess the rubbers' vulnerability to tearing and stretching.



One problem experienced with the standard flap type valve, that has been extensively used, is splitting of the rubber at the point where it is clamped. The continual movement of the valve has often been found to lead to a stress related failure at the point about which the rubber trys to hinge. This occurs most frequently when the retaining bolt holding the valve rubber is over tightened, compressing the rubber. Using a curved washer reduces the problem by not having a sharp edge about which the rubber bends and eventually is cut. The rubber instead follows a more gentle curve along its length reducing the likelihood of stress concentration and splitting of the rubber.

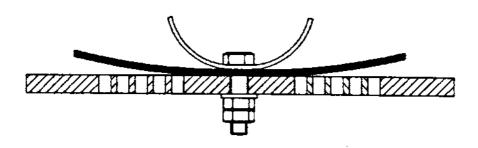


Diagram showing curved washer used in delivery valve.

Another important factor in manufacturing the rubber discs is the cutting of the central hole. This must be done cleanly with no ragged edges or flaws where cracks could start and then spread with the continual movement and stretching of the rubber. To do this it is recommended that a hole punch be bought or manufactured ensuring holes with clean edges can be accurately and repeatably made.

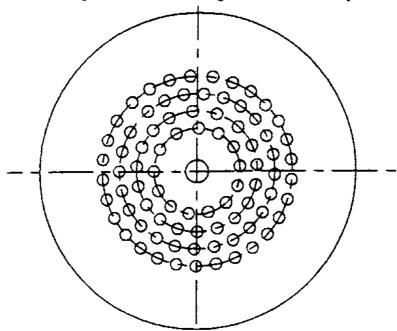


Diagram showing arrangement of delivery valve holes

The valve disc itself should be manufactured from steel plate with a minimum thickness of 3mm (10 swg) and preferably be up to 6mm. The arrangement and size of the holes in the plate is important for a number of reasons:

- 1) The hole size must be large enough to allow high flows with little resistance.
- 2) The hole size must be small enough to prevent the pressure of water in the air vessel from pushing the rubber into the holes thus deforming it and causing potential cracks.
- 3) The radius from the center in which the holes are confined needs to be as large as possible to maximise throughput but limited to allow sealing of the rubber around the outside of the valve plate.
- 4) The holes should not be too close together to prevent cracking of the valve disc between holes due to the continuous fatigue loading.

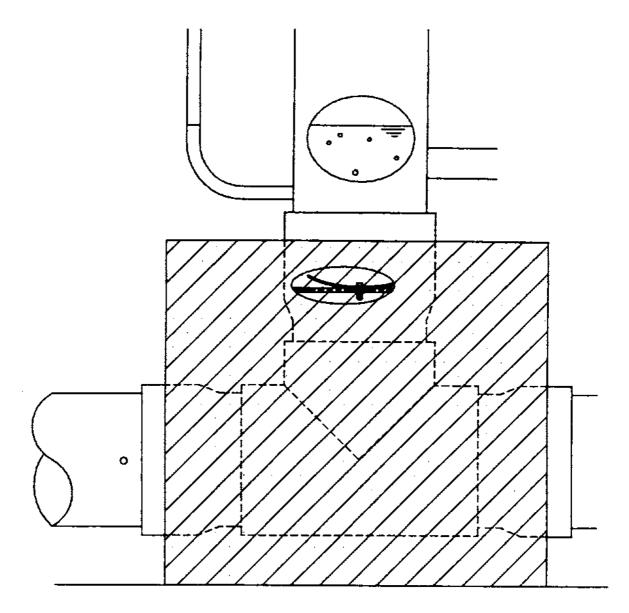
Valve plates using thick plastic material have been tested in an attempt to do without the need for a metal component. The life of such discs however was found to be too short under the loading experienced.

Marking out and accurately driling the arrangement of the large number of holes required in the valve plate can be an arduous and time consuming process. If a number of pumps are to be made it is well worth making a jig, both to cut down on the time taken and to ensure accuracy. Under the manufacturing aids section there is a drawing of one design of a valve plate jig. It ensures both the accuracy of the circumference of the plate and the accuracy of the spacing and number of holes.

### Snifter Valve

During operation of the pump, air will be constantly taken into solution at the air/water interface in the air vessel. This slowly reduces the amount of air in the air vessel leading to inefficient operation and pressure spikes significantly higher than the static delivery head. Air therefore has to be constantly and reliably introduced into the air vessel to replenish that being lost in order to keep the air vessel full and the pump working at peak efficiency. This is done by the snifter valve allowing air to enter into the body of the pump each time the pressure recoil opens the impulse valve. The slight negative pressure during the recoil phase of the cycle draws air in through the snifter valve. It is placed to enable the air to travel to the under side of the delivery valve waiting to enter the air vessel at the next delivery cycle.

There are a number of types of snifter valve that have been used on ram pumps over the years. The main design considerations are that the valve is reliable and lets in the correct amount of air each cycle. On initial start-up of the pump the volume of air in the air vessel (at atmospheric pressure) is compressed as the delivery pressure builds up. The flow of air into the air vessel from the snifter valve needs to be sufficient to re-fill the air vessel over a period of time. If too much air is entering through the snifter, the air vessel will fill up quickly and then the excess air will simply be taken up the delivery pipe where it may create problems of air locks. The snifter therefore needs to be large enough to allow sufficient air to ensure replenishment of the air vessel but not so large that the delivery pipe has a large amount of air travelling in it.



The simplest type of snifter is a hole drilled in the pump body close to the underside of the delivery valve. In the DTU M3.2 the best place for this is just upstream of the tee piece that connects the drive pipe to the pump. A small jet of water will squirt through the hole with the pressure inside the pipe until the recoil cycle occurs when air will be sucked through the hole into the pipe. As the water accelerates beginning the next cycle, some of the air rises up and sits under the delivery valve. This snifter hole should be drilled in the side of the pipe after the pump has been started for the first time.

### Use the following procedure;

- 1) On initial start-up of the pump allow it to settle and stabalise at the system delivery pressure.
- 2) Make a note of the level of the air in the air vessel using the air sight tube.
- 3) Drill a 1.5mm dia hole in the tee/pipe as specified above.
- 4) Wait for 30 mins to 1 hour to see if the amount of air changes. If the air level continues to increase until it reaches the top of the delivery pipe connection, then the snifter valve is probably about the right size. If the amount of air remains constant or reduces then increase the hole diameter to 2mm. Repeat this process until the hole is big enough to allow the air level to drop down to the delivery pipe connection.

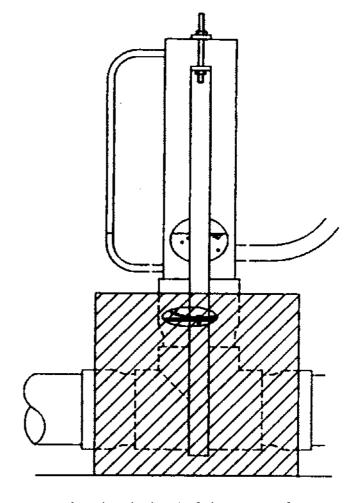
### Air Vessel Size.

Over the years that ram pumps have been used there have been a number of different theories proposed and used to design air vessels. One purpose of the air vessel is to turn the intermittent flow through the delivery valve into a steady, continous flow up the delivery pipe. The air vessel provides the pump with a constant head to pump against, limits the size of the damaging pressure spikes, and removes the inefficiencies associated with intermittent flow in the delivery pipe. The size of the air vessel therefore should ensure that conditions (ie pressure) in the air vessel are little affected by the sudden inflow of water each cycle coming through the delivery valve. The volume of air in the air

vessel therefore should be at least 20 and preferably nearer 50 times the expected delivery flow per cycle. An air vessel with a volume many times that of the water entering per cycle will experience little change in conditions at each delivery. Pumps running to low heads with large delivery flows therefore actually require air vessels larger than ones pumping smaller flows to high delivery heads.

For example; A pump delivering 30 l/min and operating at 60 cycles per minute has a flow per cycle of 0.5 litres. The minmum air vessel volume for this case should be 20 x 0.5 = 10 litres.

The design of the DTU M3.2 110mm PVC pump is attempting to use the fewest number of components possible. The air vessel has therefore been restricted to the same 110mm pipe used in the rest of the pump. This pipe typically has an internal cross sectional area of around 7500mm<sup>2</sup> and therefore a 130mm length of pipe is required per litre volume of air vessel. The maximum expected delivery flow under normal conditions is 0.5 litres per cycle requiring a 10 litre air vessel that is 1300mm long.

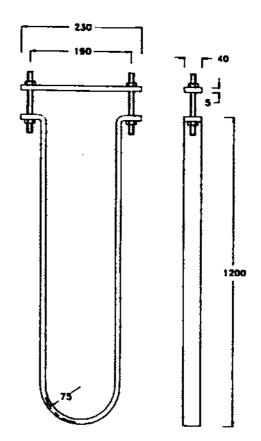


Sight tubes on an air vessel provide a very simple way of checking the level of air and therefore the effectiveness of the snifter valve. A number of problems have been encountered with the manufacture and use of air vessels that are worth mentioning:

- 1) Small bore, 'see-through' plastic tubing is not always easy to find.
- 2) Most tubing that is available deteriorates over a few months, becoming cloudy so that it is very difficult to distinguish the water level inside. Fitting a sight tube is still worthwhile under these circumstances as it is during commissioning of the pump and sizing the snifter valve that the sight tube is most useful.
- 3) Making connections onto the air vessel can be quite difficult. Reinforcing strips of pipe can be used over areas where the connections are to be made to increase the wall thickness of the pipe for glueing or threading.

### Air Vessel Strap

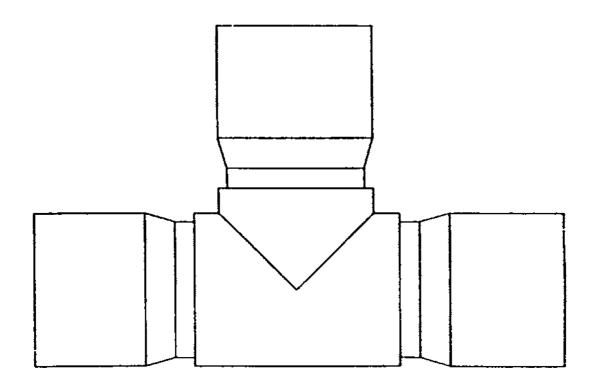
The air vessel has to be held down to prevent the pressure inside it blowing out from the tee piece. The concrete block holding the tee piece makes a good solid anchor for this strap and allows the air vessel to be securely clamped. A variety of types of clamp have been used and the one shown in the drawings section of this paper is probably the simplest.



### **Pipe Fittings**

### Tee Piece

The original design of the DTU PVC ram pump had the drive pipe connected directly with the impulse valve. The impulse valve then pushed into an elbow that was incased in concrete and fixed to the concrete pump base. The delivery valve sat in the top of the elbow and the air vessel was pushed down on top of it. With an increased understanding of pump operation and after some laboratory testing it was decided to place the delivery valve and air vessel upstream of the impulse valve. On the DTU steel pumps this had given a number of operational advantages, particularly in reducing peak pressures and so it was also applied to the plastic pumps. This altered configuration overcame some installation problems but created others.



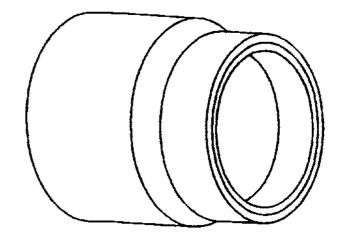
With the elbow solidly fixed downstream of the impulse valve the shocks during each pump cycle were transfered through the elbow into the concrete block. This provided good anchoring for the pump but led in some instances to cracking of the elbow. As the end of the drive pipe entering the drive tank is also fixed (and the pipe often buried) a removable section of pipe was required to allow fitting and removal of the impulse valve. This often proved to be a weak point as a good seal had to be made once the impulse valve was installed. With the revised arrangement the impulse valve is downstream of the concrete block and so provides no anchorage to prevent movement of the valve. So a further anchoring block has to be installed at the end of the impulse valve leaving enough room to allow the valve to be slid in and out of the tee piece. The gap between this second anchoring block and the valve is filled using a wedge once the valve is in place. The end of the valve also required an end cap for sealing (see below) which had to be capable of withstanding the constant shock loading. The elbow that previously experienced a substantial shock loading from the movement of the impulse valve was replaced by a tee piece that was free of this fatigue problem.

Tee fittings are commonly used in plastic pipework installations and are normally made by injection moulding. These fittings are often available in developing countries but in many cases, even where plastic pipe is manufactured, they have to be imported. They tend to be extremely expensive and are often of low quality. Experience of installations in Zimbabwe showed that the cost of a suitable tee piece was the equivalent to 3-4 meters of drive pipe - a significant cost. Such fittings were not only expensive but also in very short supply. In line with the goal of manufacturing pumps from standard pipe material a method for tee manufacture using small sections of pipe was developed. Sockets for the connection of pipes are formed by heating the ends of the pipe in an oven or oil bath and forcing them over a specially made, tapered former. Diagonal cuts are then made at 90 degress and the two sections glued together. (see drawing section). Fittings made in this way are much cheaper than those available commercially and overcome the problems of availability.

### End Cap

The new pump configuration required that the end of the impulse valve be sealed with a cap. Commercially manufactured end caps are generally available and provide a good seal. However the constant movement of the impulse valve at each pump cycle crushes the end cap between the valve body and the solid end block.

It is not possible to significantly prevent this movement as the plastic material has a high degree of flexibility and so joints tend to move under the pulsing pressure experienced in the pump. Thin walled, injection moulded end caps were found to last a very short time before cracking due to the high fatigue loading experienced. On the first site installed in Zimbabwe with this configuration a number of end caps of increasing strength were fabricated. The final solution was to make a thick walled socket using the socket former, reinforced at the end with a number of extra rings of pipe. A 5mm metal disc was then shaped to fit into the end of the socket and sealed firmly in place using plumbers putty.

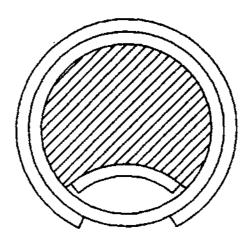


### **Drive Pipe**

### **Drive Pipe Diameter**

Throughout the DTU research into PVC ram pumps, the diameter of drive pipes used has been standard 4" 110mm O/D. Pumps have been designed specifically for this common size of pipe that has been found to be widely available in developing countries. The pump components themselves are now made almost entirely from this basic pipe material in order to reduce cost and simplify the raw material requirement.

The body of most ram pumps, and particularly the section housing the impulse valve, tend to be of a larger cross-sectional area than the recommended drive pipe. In the DTU steel designs for instance a 4" diameter body is used to match a 2" drive pipe diameter. This ensures that the frictional loss of water flowing through the impulse valve is low enough to allow sufficient flow in the drive pipe thus matching pump to drive pipe. A general rule that simplifies the initial sizing and design of an impulse valve is to ensure that, at all points through the pump body and impulse valve the area available for water flow is equal to, or greater than the area of the drive pipe. The design of the DTU PVC rams however is restricted to using the same 110mm pipe for the body of the impulse valve as is used for the drive pipe. The flow area through the holes of the valve is greater than the area of the drive pipe but at the leading edge of the tongue even at maximum stroke the flow area is reduced by around 20%. This is illustrated in the diagram below.

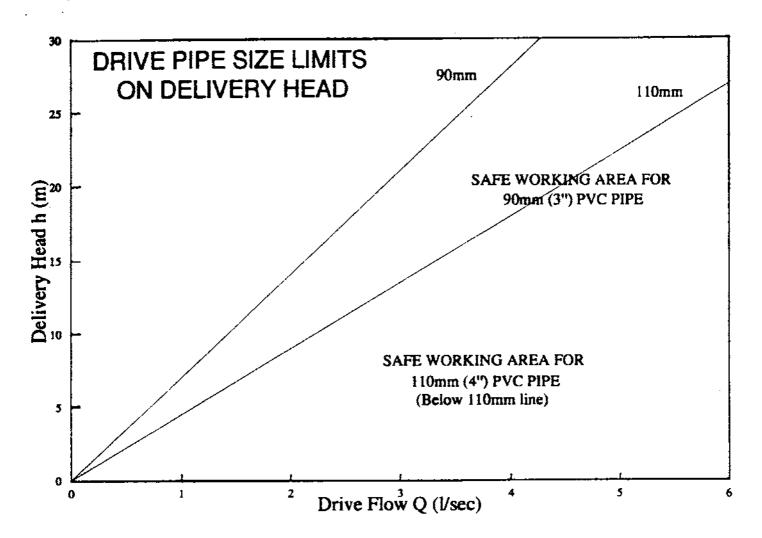


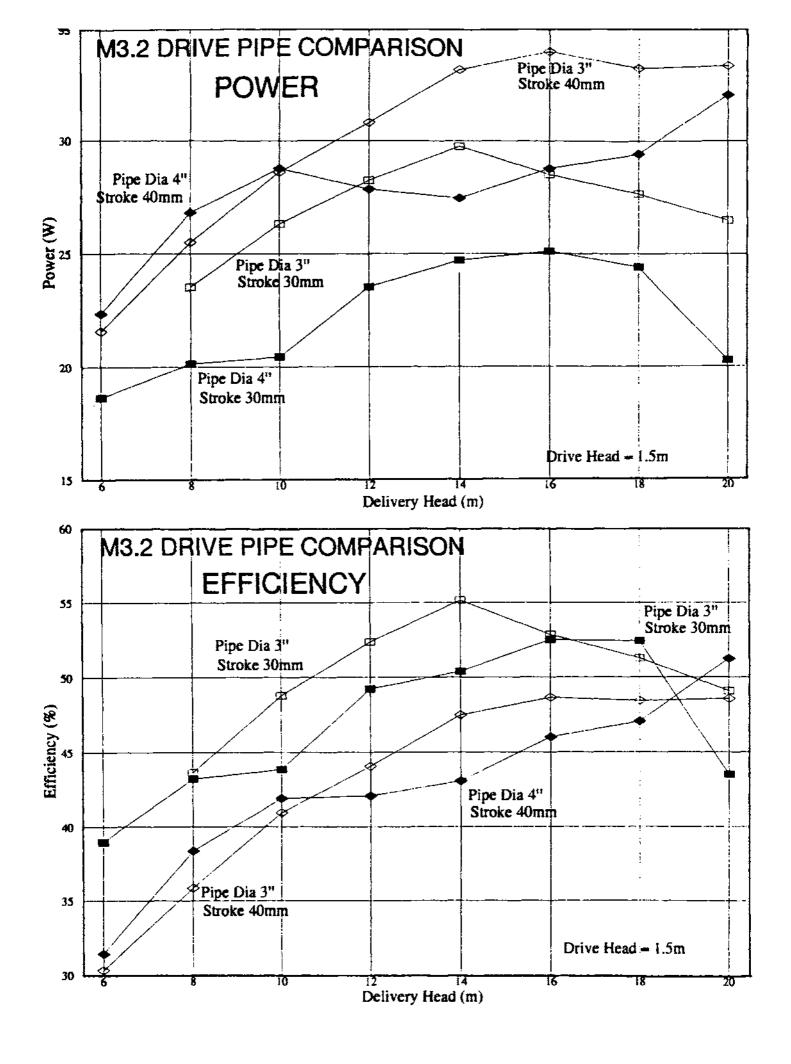
Cross-section of Impulse Valve showing restriction to flow.

Whilst it is possible to achieve drive flows in excess of 350 l/min with this arangement it became clear that particularly at low strokes the size and design of the impulse valve was not allowing full use of the diameter of the drive pipe. This situation is greatly exaggerated at lower strokes when the pump is tuned down in order to use less drive water. In effect the velocity of water in the drive pipe when the valve begins to shut is considerably lower than the maximum capacity of the pipe. As the kinetic energy available for pumping is proportional to the mass of the water and to its velocity squared, it makes sense to keep velocities high and lose a little mass by reducing pipe diameter.

Laboratory tests have been carried out in order to compare the 110mm drive pipe with the next common size down; 90mm. The results of these tests are summarised in Graph Nos X,X and show quite clearly that under most conditions both the efficiency and power output of the pump are improved by using the smaller drive pipe size.

Whilst the pump will work perfectly well with a 110mm drive pipe over the complete range of operating conditions it is now recommended that a 90mm pipe be used if available. This may also give a small saving in system cost and gives a greater potential range of pipe that can be used if one size is not available. In situations of particularly low drive flow the pump may not actually be able to operate with the larger sizes of drive pipe. The maximum head to which a pump can deliver is dependant upon the velocity of the water in the drive pipe. To reach a given delivery head there has to be a corresponding drop in velocity turning kinetic energy to potential energy. If the velocity drop required to reach a given pressure is larger than the maximum velocity of the water in the drive pipe then the pump will never reach the required delivery head although it can appear to be operating. Smaller diameter drive pipes will have a higher water velocity for a given flow and therefore will permit operation in situations where larger diameter pipes would not work. The graph below shows the typical lower boundary of the commonest pipes used for DTU M3.2 PVC pumps

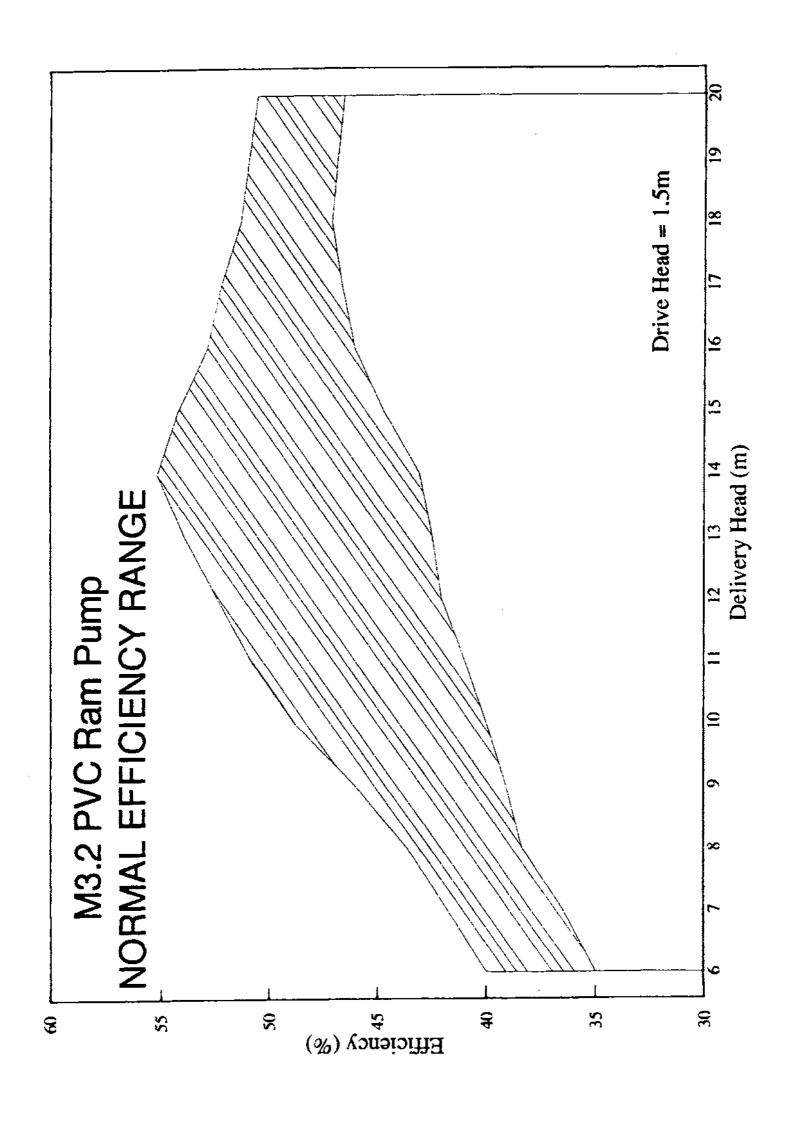


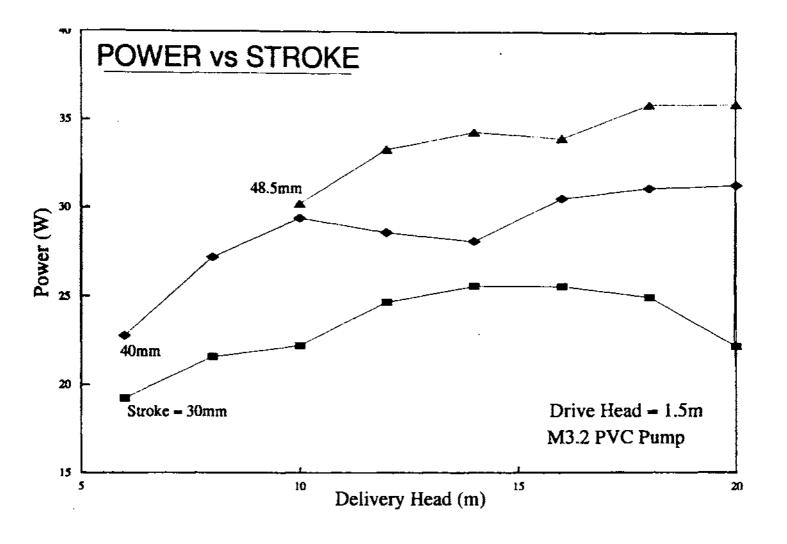


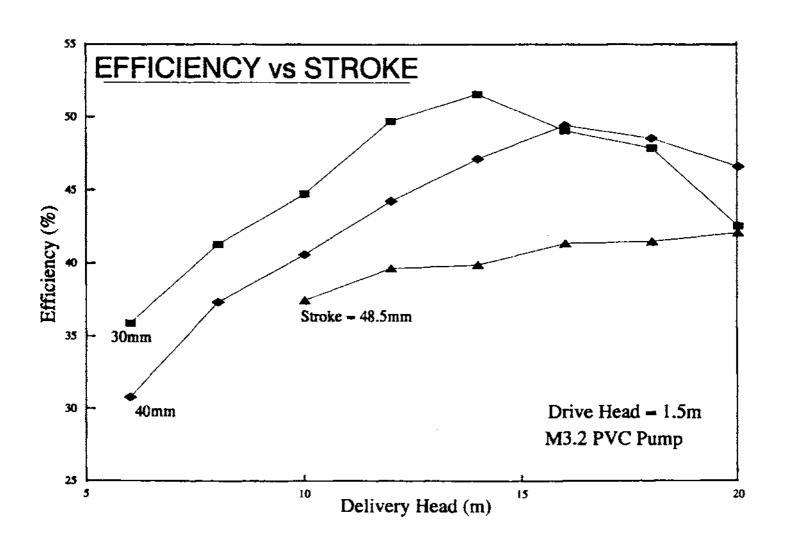
### **Drive Pipe Length**

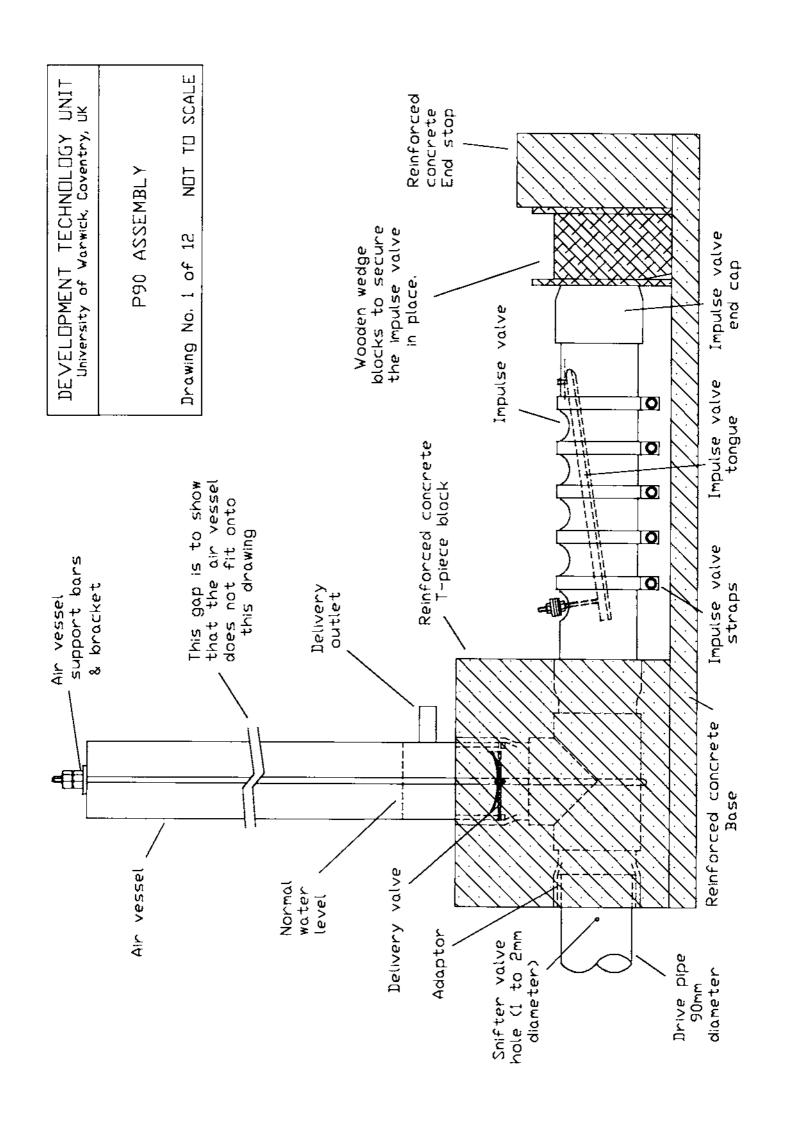
One critical factor with PVC ram pumps for small irrigation schemes is cost. The pump and system constraints have been designed to give good performance, reliability, local manufacture, availability of spare parts, all for the smallest possible cost. One of the major cost components of any ram pump system is the drive pipe which can often equal or even exceed the cost of the pump unit itself! As drive heads are comparatively small for PVC pumps, the physical layout of the site can often allow drive pipe lengths to be very short. Systems have been installed and successfully run with drive pipe lengths of only 6m. Plastic pumps generally can utilise shorter drive pipes than their steel equivalents due to the much lower wave speeds of the transients moving in them. Longer drive pipes can increase the pumping energy available by increasing the mass of water moving in the drive pipe and increasing the length of the delivery cycle during operation. Longer drive pipes introduce greater friction into the system so that less of the drive head is available to the pump. This consideration of pipe friction imposes an upper limit on the length of drive pipe that can be used for a given drive head.

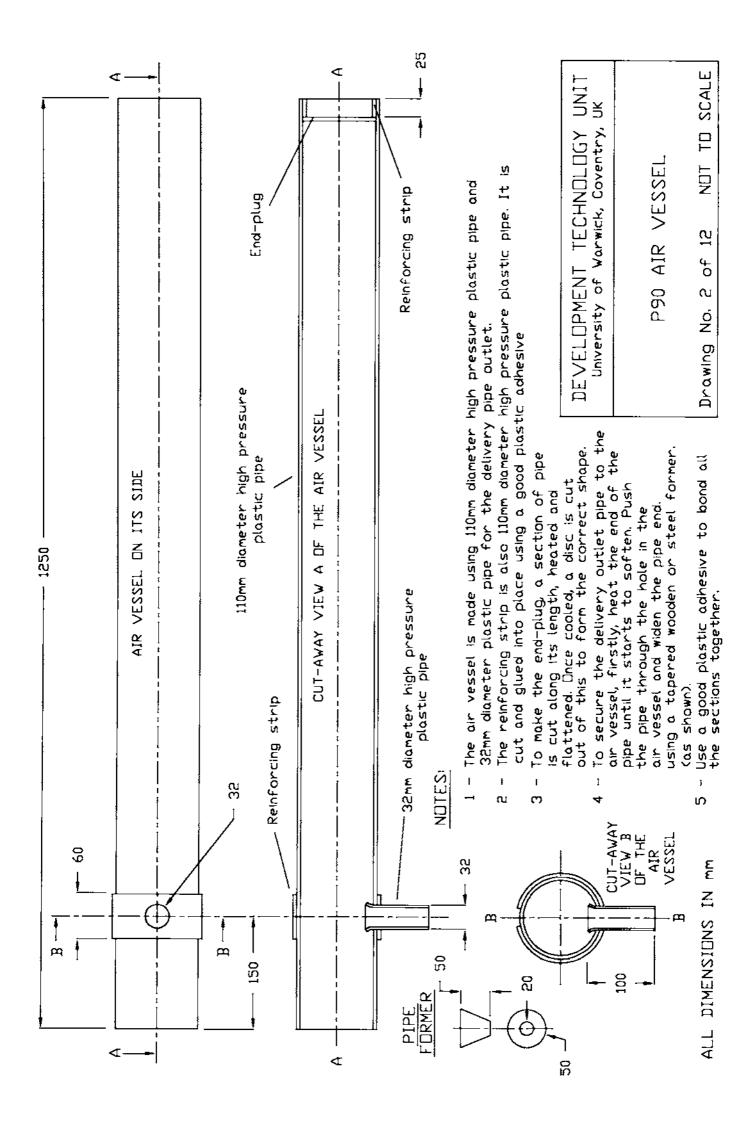
Bearing the all important cost factor in mind it is recommended that drive pipe length normally be kept in the range 6 to 30m with 12m being a rough guide to the optimum when balancing cost and performance. If a combination of a necessarily long drive pipe (greater than 20m), high drive flow (greater than 300l/min), and low delivery head (less than 8m) occurs it is recommended that a 110mm rather than the standard 90mm drive pipe be used as the friction in a 90mm pipe would be more significant in such a situation.

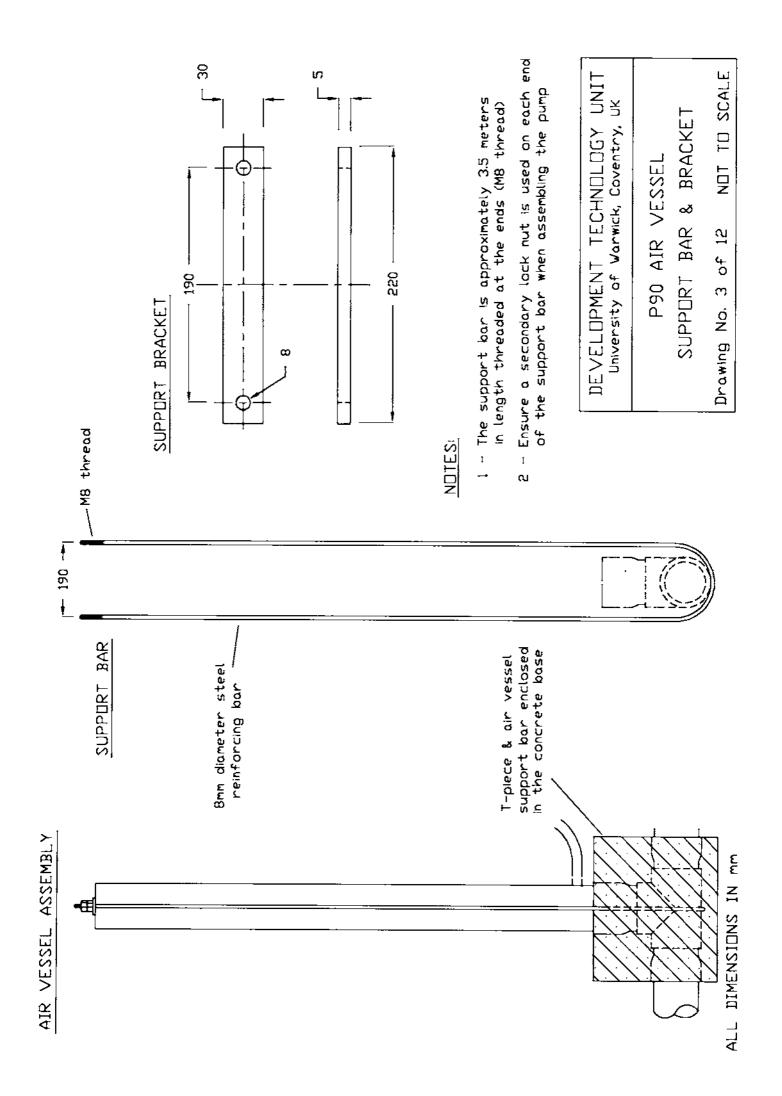


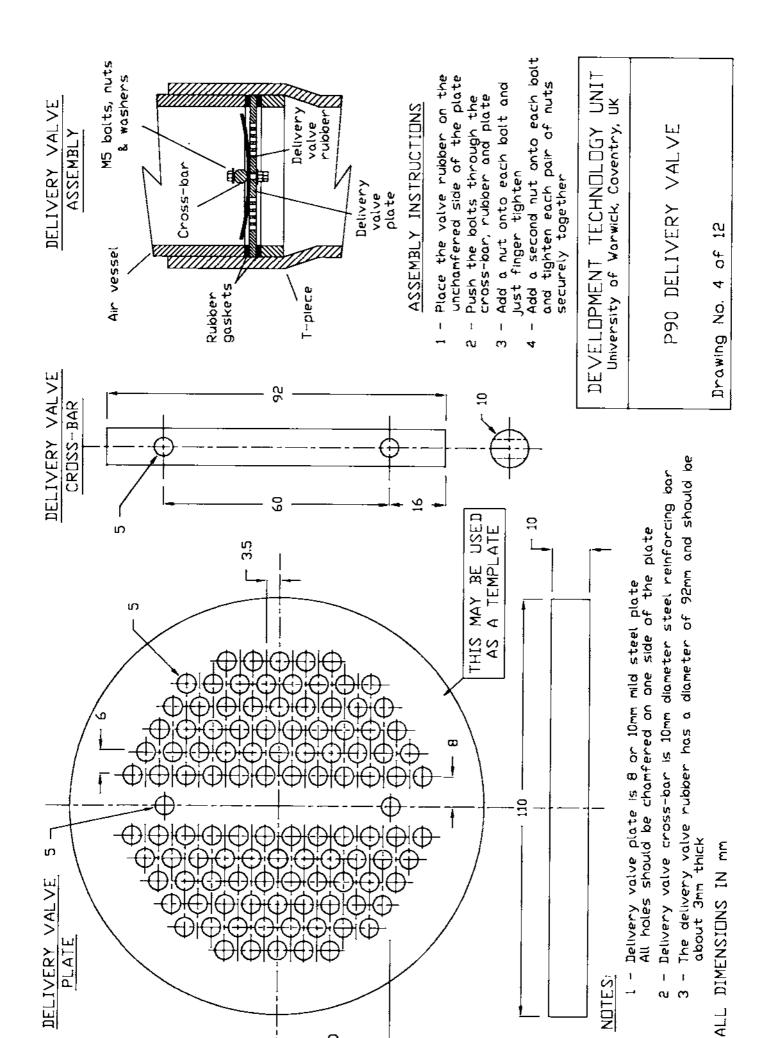


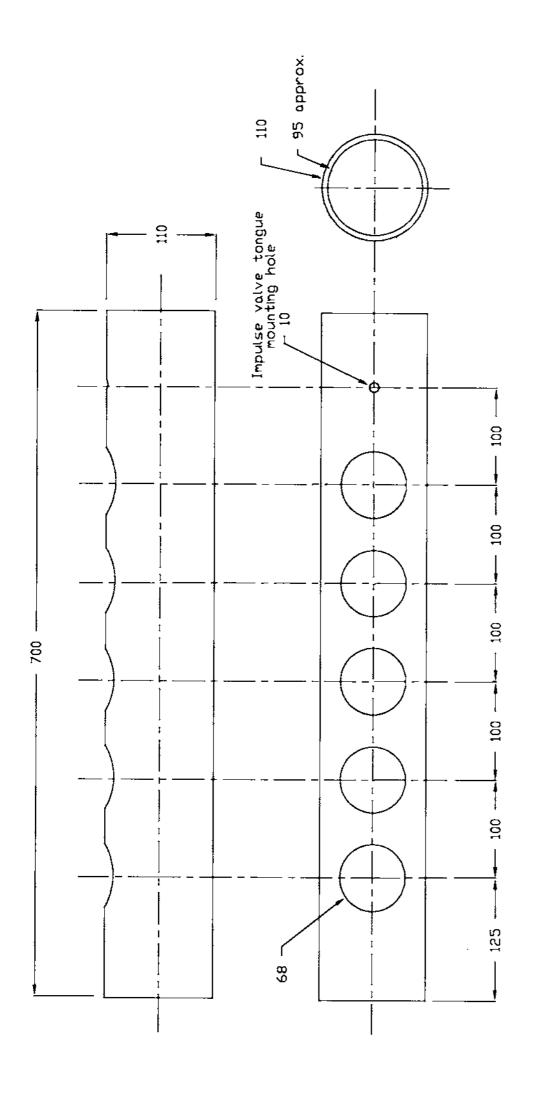












# DEVELOPMENT TECHNOLOGY UNIT

high pressure PVC pipe. The wall thickness of the pipe

is usually about 7mm.

2 - A tank cutter of between 66 and 70mm may be used to cut out the large impulse valve holes.

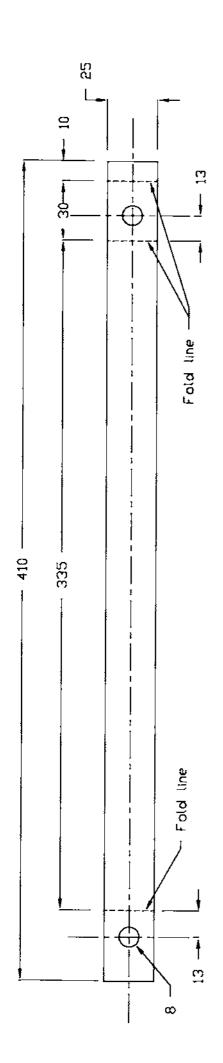
1 - The material used for the impulse valve is CLASS 16

NOTES

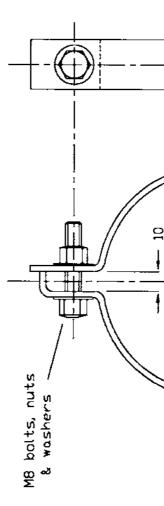
P90 IMPULSE VALVE

NDT TO SCALE Drawing No. 5 of 12

ALL DIMENSIONS IN MM



# ASSEMBLED IMPULSE VALVE STRAP



### NOTES

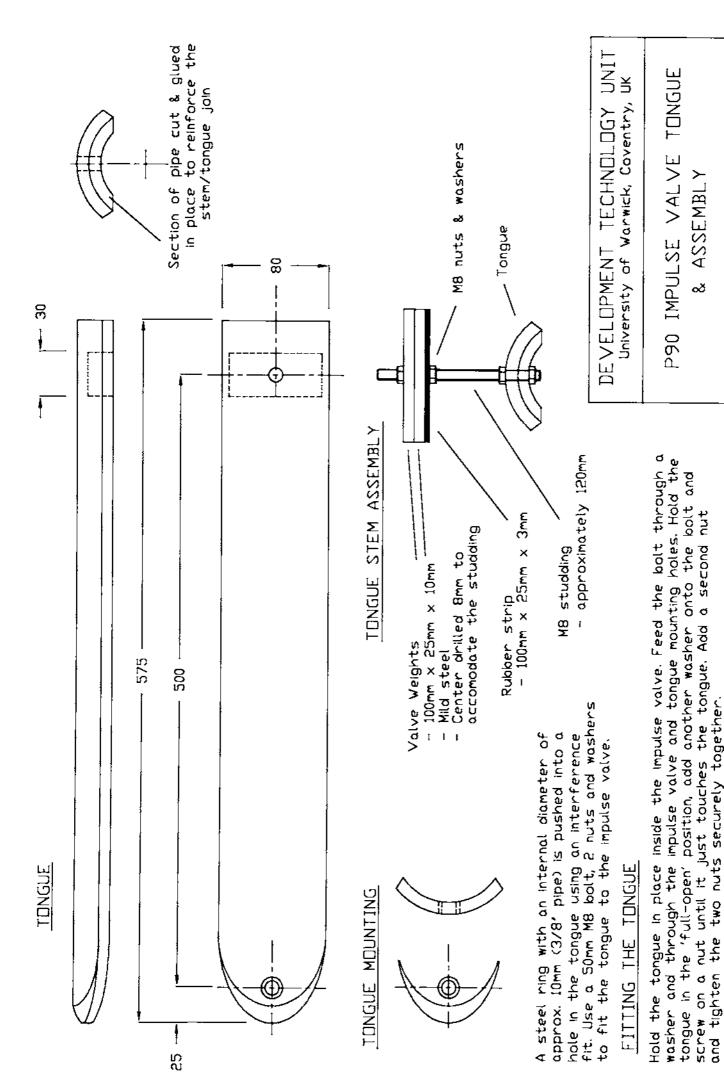
- 1 The material used to make the strap is 25 x 3mm mild steel.
- 2 5 straps are needed for the impulse valve.
- 3 Mark the measured fold lines on the cut lengths of steel, After folding the straps wrap them around the impulse valve and check that there is a minimum gap of about 10mm between the folded up-rights.
- 4 When the straps are assembled, paint them before adding them to the impulse valve.

# DEVELOPMENT TECHNOLOGY UNIT University of Warwick, Coventry, UK

### P90 IMPULSE VALVE STRAP

Drawing No. 6 of 12 NOT TO SCALE

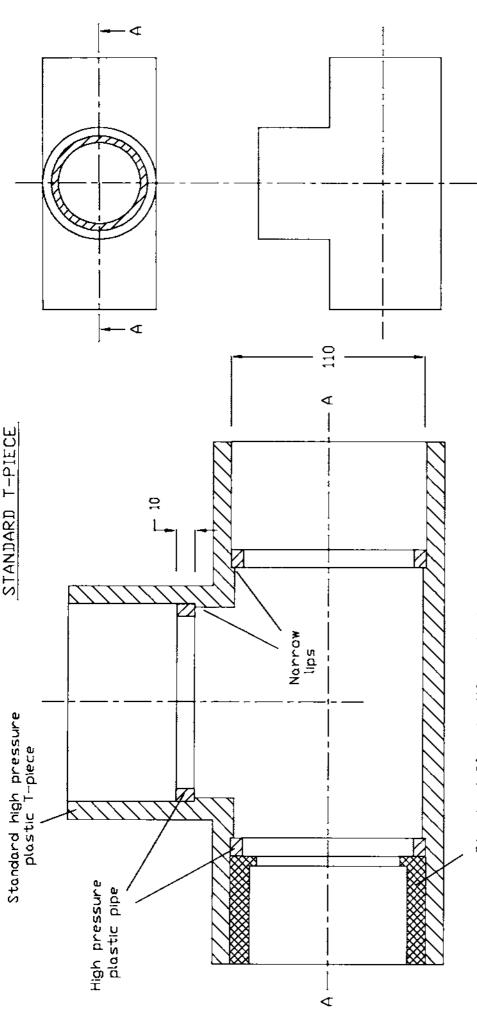
ALL DIMENSIONS IN MM



ALL DIMENSIONS IN MM

NOT TO SCALE

Drawing No. 7 of 12



# Standard 90mm to 110mm adaptor

### NOTES

- by hand. The drawing above shows an example of a commercial T-piece (high pressure plastic) that is suitable for 110mm diameter pipe, The T-piece for the P90 may be bought commercially or made
  - gluing into place a 10mm length of high pressure plastic pipe as shown. T-pieces available on the market tend to have narrow support lips as shown above. These need to be reinforced and this is done by 1 Ω.
- đ When purchasing a 110mm high pressure plastic Tapiece, also buy 90mm to 110mm adaptor. This is because the drive pipe for the pump has a 90mm diameter and will have to be adapted to fit the T-piece. 1 ന

# ALL DIMENSIONS IN AR

# DEVELOPMENT TECHNOLOGY UNIT University of Warwick, Coventry, UK

## P90 - USING A STANDARD T-PIECE & ADAPTOR

Drawing No. 8 of 12 NDT TD SCALE

## MAKING A T-PIECE

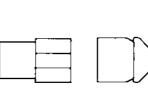
## PART A

Dpen the heated shorter pipe and fit it over the center of the Cut the shorter pipe down its length and heat it until workable. Cut 150 & 400mm lengths of pipe. longer section using glue and clamp it in place.

'V~Notch as shown, Make sure the gap on the shorter outter pipe Using the T-piece former, form sockets at each end of PART A. Next, cut out a 90 degree

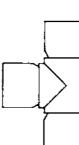
is apposite the WV-Notch'

PART B



longer. Cut a piece of pipe to fit the gap left on the outer pipe. Cut 75 & 200mm lengths of pipe. Cut, heat & glue the shorter pipe flush with one end of the Heat & glue this into place.

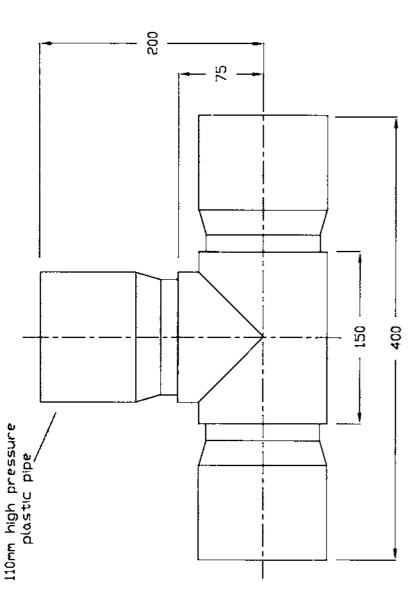
Form the socket on the end of PART B and cut the other end to fit the 'V-Notch' on PART A.



Glue together both parts using a mixture of PVC glue and pipe shavings to fill the gaps. File both PARTS A & B until a reasonable fit is obtained.

Wine may be wrapped around the The T-piece is now ready to be glued parts to hold them more set into a concrete base. securely together.

## COMPLETED T-PIECE



The drive pipe for the P90 has a diameter of 90mm. Therefore, to fit the drive pipe into this T-piece, a 100mm to 90mm adaptor should be purchased or made up using available pipe. NOTE

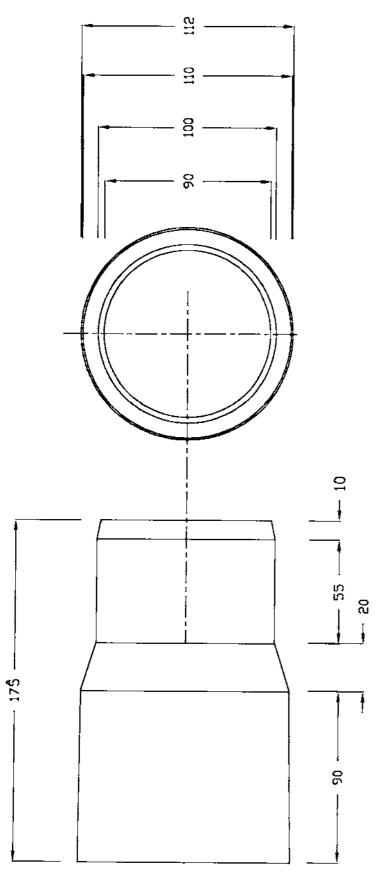
DEVELOPMENT TECHNOLOGY UNIT University of Warwick, Coventry,

MANUFACTURE P90 T-PIECE

NOT TO SCALE Drawing No. 9 of 12

ALL DIMENSIONS IN MM

Vire



### NOTES

- 1 This socket former is designed to be used with 110mm outside diameter plastic pipe.
  - 2 This former may be made from steel, aluminium or wood.
- 3 The former is used to to make both the pump T-piece and End cap.

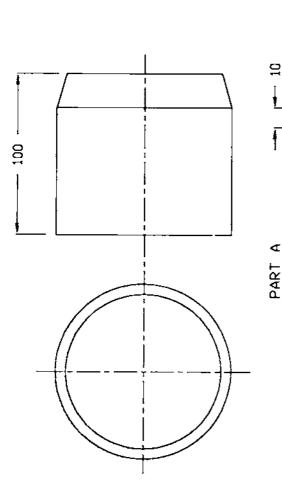
# INSTRUCTIONS FOR USE

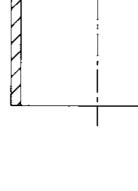
- $1\,\sim\,$  The first step is to heat up the plastic pipe to make it soft and workable. This may be done by immersing the pipe in hot oil at about 130 C or by rotating the pipe slowly over a heat source.
- 2 When the pipe is soft enough push it quickly and firmly over the former.
- 3 Let the pipe cool and harden before removing it from the former.

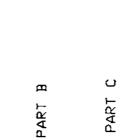
ALL DIMENSIONS IN MM

DEVELOPMENT TECHNOLOGY UNIT University of Warwick, Coventry, UK	P90 SOCKET FORMER	Drawing No. 10 of 12 NOT TO SCALE

# MAKING AN END CAP







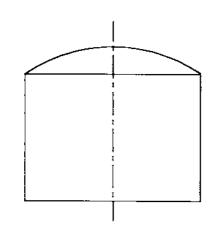
NOTE

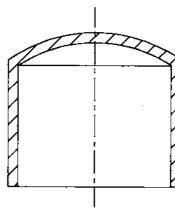
# MANUFACTURE INSTRUCTIONS

- Cut a 100mm length of high pressure plastic pipe and heat it as per the socket former instructions.
  - Push the softened pipe quickly and firmly over the socket former to shape PART A. ณ
- PART B, the end cap plug, and PART C, the reinforcing strip are made by the same methods used to make the Air vessel. When PART A has cooled, use a good plastic adhesive to glue in the reinforcing strip followed by the end cap disc. When dry the end is ready for use

ALL DIMENSIONS IN MM

## STANDARD END CAP



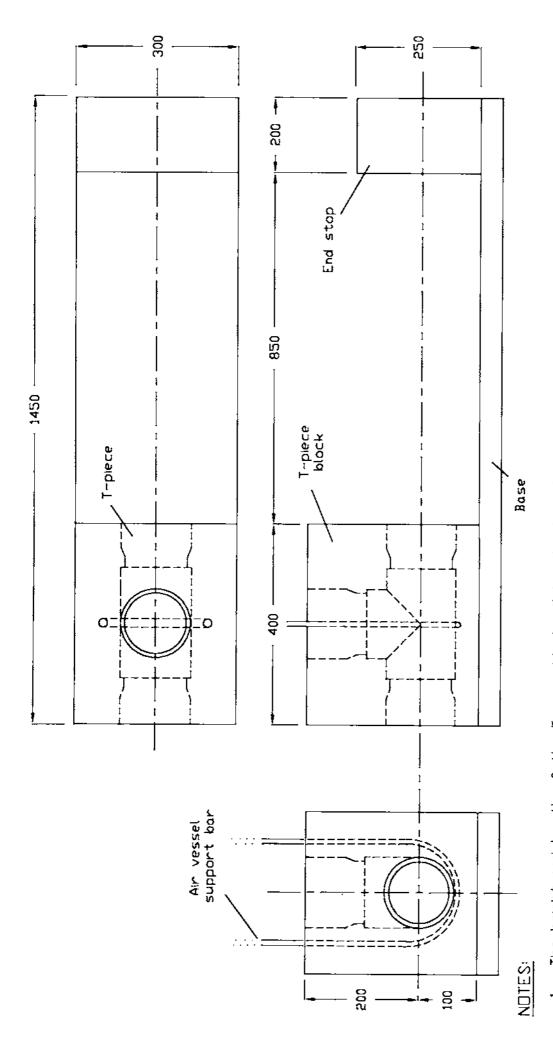


The End cap may be purchased commercially or made as shown.

### TECHNOLOGY UNIT University of Warwick, Coventry, UK DEVELOPMENT

### P90 IMPULSE VALVE END CAP

NOT TO SCALE Drawing No. 11 of 12



1 — The height and length of the T-piece block will be shorter when a standard T-piece is used make sure the bottom of the T-piece is about  $50\,\mathrm{mm}$  above the top of the base.

- 2 The depth of the base should be at least 75mm. The depth may be greater If a more solid foundation is needed.
- 3 Use steel reinforcing in the base, T-piece block and end stop to join the three sections together and to reinforce each section. A local builder will know how to do this.

DEVELOPMENT TECHNOLOGY UNIT University of Warwick, Coventry, UK

P90 REINFORCED CONCRETE
BASE, T-PIECE BLOCK
& END STOP
Drawing No. 12 of 12 NOT TO SCALE

ALL DIMENSIONS IN MM